Influence of Gradient and Smoothness of Atrial Wall Thickness on Initiation and Maintenance of Atrial Fibrillation

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Abstract

This work uses a highly detailed computational model of human atria to investigate the effect of spatial gradient and smoothing of atrial wall thickness on inducibility and maintenance of atrial fibrillation (AF) episodes. An atrial model with homogeneous thickness (HO) was used as baseline for the generation of different atrial models including either a low (LG) or high thickness gradient between left/right atrial free wall and the other regions. Since the model with high spatial gradient presented non-natural sharp edges between regions, either 1 (HG1) or 2 (HG2) Laplacian smoothing iterations were applied. Arrhythmic episodes were initiated using a rapid pacing protocol and long-living rotors were detected and tracked over time. Thresholds optimised with receiver operating characteristic analysis were used to define high gradient/curvature regions. Greater spatial gradients increased the atrial model inducibility and unveiled additional regions vulnerable to maintain AF drivers. In the models with heterogeneous wall thickness (LG, HG2 and HG1), 73.5 \pm 8.7\% of the long living rotors were found in areas within 1.5 mm from nodes with high thickness gradient, and 85.0 \pm 3.4\% in areas around high endocardial curvature. These findings promote wall thickness gradient and endocardial curvature as measures of AF vulnerability.

1. Introduction

Atrial fibrillation (AF) is a frequent and progressive heart condition correlated with high morbidity and mortality. The lack of basic understanding of underlying atrial dysfunctional and structural substrates may be the cause of the low success rate in treatment of persistent AF patients. Computational heart modelling could aid the development of quantitative tools to evaluate the influence of structural features on AF vulnerability.

Recent theoretical studies have highlighted the effect of surface curvature \cite{1} and tissue gradient \cite{2} on the dynamics of re-entrant drivers (RDs). The anchoring of scroll waves to regions with heterogeneous atrial wall thickness have been proven both experimentally and computationally \cite{3}. However, simplified models were used and no detailed atrial model have been exploited to assess correlation between these structural features and regions vulnerable to initiate and maintain AF.

We hypothesized that heterogeneous thickness influences both initiation and maintenance of AF episodes. Moreover, we sought to investigate the drift of meandering scroll waves along regions of large spatial gradients in wall thickness.

2. Methods

2.1. Atrial models generation

In this work, a highly detailed volumetric bi-atrial geometry derived from magnetic resonance images was used \cite{4}. The volumetric mesh had an average edge length of 0.4 mm and a homogeneous wall thickness (HO) of 3 mm. This model was used as baseline for the generation of 3 model variants varying the regional myocardial thickness and the smoothness between the different regions of the atria. The heterogeneous myocardial thickness was introduced following the method proposed in \cite{5} consisting in moving the endocardial nodes in the normal direction until the desired Euclidean distance between the endocardial node and the closest node on the epicardium is reached. The regional thickness ranges were taken from \cite{6–8} and are shown in Fig. 1. The blue stars mark the final regional thickness value for the model with low gradient (LG) between the left/right atrial wall (LAW)/(RAW) and the other regions. The thickness values in the model with a high gradient between LAW/RAW and the other regions are indicated by red stars. Moreover, since the latter model entailed unrealistically sharp edges at the transition between regions with highly different thickness, we ap-
plied 1 iteration (HG1) or 2 iterations (HG2) of Laplacian smoothing to the endocardial surface.

Fiber orientation was calculated by a semi-automatic rule-based algorithm [9]. A variant of the Courtemanche et al. model reflecting atrial fibrillation-induced remodeling was used as ionic model [10]. Nine regions with different anisotropy ratio were implemented to consider the heterogeneity in the atria [11]. Conductivities of all models were tuned to reach a last sinus rhythm activation time of 160 ms and a global longitudinal conduction velocity of 0.7 m/s. The spreading of the electrical wave along the myocardium was simulated by solving the monodomain system using openCARP/CARP [12].

2.2. Thickness gradient and endocardial curvature

To better identify the cause of scroll wave drifting, we computed two thickness features: thickness gradient and endocardial curvature. The curvature of the endocardial surface at each node was calculated as $1/R$, where $R$ is the radius of the fitted osculating sphere.

2.3. Protocol to test inducibility

We tested inducibility of arrhythmic episodes by pacing from 48 evenly distributed points on the endocardial surface with an inter-point distance of 2 cm. The rapid pacing protocol consisted in a train of pulses with decreasing coupling interval from 160 ms to 110 ms. We considered a point to be ‘inducing’ if by pacing from that location, an arrhythmia was induced and sustained for at least 1.5 s after the last beat of the pacing protocol.

2.4. Detection and tracking of AF dynamics

Reentrant waves have an organising center in many cases. In 3D this is known as filament, which represents the center-line of a scroll wave. We followed the method presented in [13] to detect filaments and we tracked the spatio-temporal behavior of each filament along the whole episode duration. We defined long-living rotors as filaments sustained for at least 500 ms.

2.5. Optimal threshold for high thickness gradient and endocardial curvature

An iterative binary classification (filaments present vs. not present) was computed to create receiver operating characteristic (ROC) curves. Thickness gradient and endocardial curvature were used as discriminators for the ROC curves. The optimum operating point on the ROC curve was defined as the point on the curve with the shortest distance to the top left corner of the graph and it was selected as threshold.

3. Results and Discussion

3.1. Inducibility

In model HO, 12 points were ‘inducing’ (10 lead to macro reentries, 2 to micro reentries). We observed 13 ‘inducing’ points in model LG (10 macro reentries, 3 rotors) and 16 points in model HG1 (6 macro, 10 micro). Furthermore, we identified 16 ‘inducing’ points in model HG2 (11 macro, 5 rotors). Number and location of the ‘inducing’ points for each model are summarized in Tab.1. The models with higher gradient between LAW/RAW and the other regions (HG1 and HG2) were more vulnerable regarding initiation of reentrant episodes compared with models with more homogeneous thickness (HO and LG). We observed the development of microreentries when pacing precisely in the areas with high thickness gradient. Moreover, the combination of high gradient and sharper edges (model HG1) had the highest number of points inducing rotors.
Table 1. Number of point inducing reentrant arrhythmic episodes in each model classified in macro reentry and micro reentry. The points inducing micro reentries are further divided per location.

<table>
<thead>
<tr>
<th>Model</th>
<th>Macoreentries</th>
<th>Microreentries</th>
</tr>
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<tbody>
<tr>
<td>HO</td>
<td>10</td>
<td>2</td>
</tr>
<tr>
<td>LG</td>
<td>10</td>
<td>3</td>
</tr>
<tr>
<td>HG1</td>
<td>6</td>
<td>5 1 3 1</td>
</tr>
<tr>
<td>HG2</td>
<td>11</td>
<td>2 2 1</td>
</tr>
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</table>

In the models HG1 and HG2, we identified more reentrant wave meandering following the PMs or the MV and, finally, being maintained close to the steps between RAW and CS, CT or RAA, as shown in Fig. 3. We found a total of 11 and 16 long-living rotors maintaining in average for 1021.5 ms and 982.5 ms in the models HG2 and HG1, respectively. Nodes in which a long-living rotor was found (see Fig. 4), mostly corresponded to locations with high gradient magnitude and surface curvature (see Fig. 4). We detected 70.5%/78.7%/71.3% of filaments in areas within 1.5 mm from the regions with high thickness gradient and 81.1%/87.1%/86.9% of filaments in areas within 1.5 mm from the regions with high endocardial curvature, in the models LG, HG2 and HG1 respectively. The optimal thresholds extracted from the ROC curves were 0.1/0.2/0.46 mm/mm for the gradient magnitude and 0.7/0.8/0.96 mm$^{-1}$ for the curvature, for the models LO, HG2 and HG1 respectively. In our simulations, no fibrotic tissue was included to clearly analyse the effect of anatomical thickness features on reentry dynamics.

4. Conclusion

In this work, we showed that the gradient and the degree of smoothing of anatomical thickness influence both the vulnerability to initiate and to maintain atrial fibrillation episodes. We presented how thickness heterogeneity increased not only the number of pacing location from which it was possible to induce an arrhythmia but also the complexity of the arrhythmia, developing more micro reentries. The inclusion of higher gradient highlighted pathways followed by meandering rotors (PMs), as shown experimentally [14] and unveiled new areas vulnerable to sustain drivers (CS and MV). Furthermore, we showed how rotors are attracted by steep edges and are drifting to the border between regions with different thickness, as theoretically predicted in [2]. Furthermore, we noticed that the degree of smoothing affected inducibility, increasing the number of points initiating rotors, and sustainability, leading to a higher number of long-living drivers. We conclude that wall thickness gradient and curvature could be valuable a priori measures to assess AF vulnerability and predict maintenance areas to ablate.

Acknowledgments

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Figure 4. Model HG1: A) endocardial nodes in which a long-living rotor was encountered are shown in red; B) thickness gradient magnitude; C) endocardial curvature showed as inverse of the osculating sphere radius. Crista terminalis and pectinate muscles view.

References


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