

Closed-loop Kinesthetic Stimulation for the Treatment of Sleep Apnea Syndromes

D. Pérez^{1,2}, G. Guerrero^{1,2}, D. Feuerstein³, L. Graindorge³, A. Amblard³, J-L. Pépin⁴, L. Senhadji^{1,2}, A. I. Hernández^{1,2}

¹INSERM, U1099, Rennes, F-35000, France

²Université de Rennes 1, LTSI, Rennes, F-35000, France

³Sorin CRM SAS (a LivaNova company), Clamart, France

⁴Univ Grenoble Alpes, CHU Grenoble, Sect Physiol Sommeil & Exercice, Inserm U1042, Pole Thorax & Vaisseaux, Lab EFCR, F-38000 Grenoble, France

Abstract

Sleep apnea syndrome (SAS) is a common disease characterized by recurrent episodes of breathing pauses or important reductions in respiratory amplitude during patient's sleep. These episodes provoke significant cardiorespiratory modifications that may have long-term cardiovascular consequences. This paper proposes a novel approach for the treatment of SAS, based on a closed-loop kinesthetic stimulation, adapted as a function of the patient's physiological response. The closed-loop control system is based on concurrent, coupled proportional-derivative (PD) controllers that modulate the stimulation amplitude delivered to the patient. The controller was tested on a first phase of a clinical protocol including 12 patients with previously diagnosed SAS. Results from one patient are presented in this paper, showing how the proposed controller is capable to adapt stimulation parameters, converging to a minimum patient-specific amplitude. These results are encouraging regarding the feasibility of the integration of the proposed controller into the therapy for the adaptive optimization of the kinesthetic stimulation amplitude and warrant a second phase of the clinical study of this system.

1. Introduction

Sleep apnea syndrome (SAS) is a common disease characterized by recurrent episodes of breathing pauses (apnea) or important reductions in respiratory amplitude (hypopnea) during patient's sleep. Although this syndrome affects more than 5% of the general population [1], it remains under-diagnosed. SAS provoke an alteration of the sleep structure (sleep fragmentation), as well as acute cardiorespiratory responses, that have been associated with chronic pathologies such as hypertension and certain metabolic

disorders [2][3]. The current recommended treatment for patients suffering SAS is the continuous positive airway pressure (CPAP) therapy [4]. However, patient compliance to this therapy is low, with an average adherence rate between 39% and 50% [5].

We have recently proposed a novel system (PASITHEA) for real-time monitoring and treatment of SAS, based on triggered kinesthetic stimulation. This system triggers a mechanical stimulation applied to the skin of the patient when apnea or hypopnea events are detected by an automatic, real-time respiratory detector. The system is composed of three elements: i) a modified cardiorespiratory ambulatory recorder (Holter) based on the commercially available Sorin Holter system (SORIN CRM, Clamart, France), for real-time acquisition, recording and wireless transmission of two electrocardiogram (ECG) channels, nasal pressure (NP) and blood oxygen saturation (SaO₂) during a whole night; ii) a kinesthetic stimulation system (LTSI INSERM U1099, Rennes, France) and iii) a real-time control application for adaptive kinesthetic stimulation, running in a standard computer. These elements communicate through a wireless communication protocol.

A complete description of the original PASITHEA system, along with preliminary results from its first clinical evaluation has been recently published [6]. This first evaluation was based on an "on-off" control algorithm, which triggers the kinesthetic stimulation as a function of respiratory event detections. Also, the stimulation parameters (amplitude, burst duration, silent interval, maximum number of bursts) were empirically fixed for all patients. Results showed that the patients who responded to therapy presented a reduced duration of respiratory events and an attenuation of the consequent hypoxia events and acute cardiorespiratory responses during the periods in which the therapy was active. However, not all patients responded correctly to the therapy. We hypothesize that these non-

responders may be minimized with the integration of a closed-loop control, capable to adapt and personalize stimulation parameters. In this work, we propose the integration of such a real-time closed-loop control method, as an improvement of the original system. Preliminary results based on data acquired from the first phase of a clinical evaluation protocol are also presented.

2. Method

2.1. Controller description

A closed-loop control system, integrating concurrent, coupled proportional-derivative (PD) controllers is proposed in this work to manage the kinesthetic stimulation amplitude delivered to the patient by the therapeutic system. The control system is composed of three main modules operating in real-time: i) a signal processing module, ii) control activation and iii) the coupled PD controller.

The signal processing module (Fig. 1) performs data processing on input signals which are: i) the NP signal, ii) one ECG lead and iii) the SaO2 signal. QRS detection is performed on the ECG signal and the instantaneous heart rate (HR), as well as the ΔHR signal are derived. The SaO2 signal is delayed and low-pass filtered (FSaO2), to then calculate its derivative. This pre-processing is applied in order to compensate for the fact that the consequences of respiratory events on the SaO2 signal are observed after a certain physiological delay. The NP signal is processed by a real-time apnea/hypopnea detector which has three possible outputs: no apnea/hypopnea detected, apnea detected and hypopnea detected. A complete description of the apnea/hypopnea detector was published in [7].

The control activation module enables the coupled PD controller module when it receives as input an apnea or hypopnea detection and will disable it in case of a return to normal respiration. Five control variables are presented as input to the coupled PD controller: i) the event duration signal (TResp) which represents the time spent from the detection instant of the current event to the current time instant, ii) ΔHR , iii) $\frac{\partial \Delta HR}{\partial t}$, iv) FSaO2 signal and v) $\frac{\partial FSaO2}{\partial t}$. The coupled PD controller module synthesizes a signal, with an amplitude modulated by the controller's output, that will be used to drive the kinesthetic actuator. This modulated amplitude has a percentage range between 0% and 100%, which is translated by the system to the specific input signal value to generate the equivalent acceleration delivered by the actuator (100% amplitude (2V RMS) typically corresponds to a normalized acceleration of 13.7 m/s^2). In addition, the synthesized signal is delivered in a burst sequence of 4 bursts with a fixed stimulation duration of 3 seconds followed by a silent period of 2 seconds.

2.2. Closed-loop algorithm

Figure 1 shows a diagram of the closed-loop control algorithm. The loop is executed in real-time and all the variables are constantly calculated. The time passed since the beginning of the application is stored in variable t while the event number for each detection is stored in e ($e = 1, 2, \dots, N$), where N is the total number of respiratory events during the whole night. The beginning, t_e^{start} and end t_e^{end} of each respiratory event e are also available variables. When an event detection e arrives, the amplitude of the stimulation burst at each time instant ($A(t, e)$) is obtained by the following equations:

$$A(t+1, e) = A(t, e) + a_1 TResp(t, e) + b_1 \Delta HR(t, e) + b_2 \frac{\partial \Delta HR(t, e)}{\partial t} + c_1 (100 - FSaO2(t, e)) + c_2 \frac{\partial FSaO2(t, e)}{\partial t} \quad (1)$$

$$A(t_{e+1}^{start}) = f_1 = \begin{cases} A(t_e^{end}) - A(t_e^{end}) * 0.1 & \text{if } TResp(t_e^{end}) < 9 \\ A(t_e^{end}) + A(t_e^{end}) * 0.1 & \text{if } TResp(t_e^{end}) \geq 9 \end{cases} \quad (2)$$

$$TResp = f_2 = t - t_e^{start} \quad (3)$$

$$A(t+1, e) = \max(20, A(t+1, e)) \quad (4)$$

$$A(t+1, e) = \min(100, A(t+1, e)) \quad (5)$$

where a_1, b_1, b_2, c_1, c_2 are the control coefficients, to be optimized.

2.3. Preliminary evaluation

A two-phases clinical study, approved by the ethics committee of the Grenoble University Hospital (EKINOX study) was designed to evaluate the proposed adaptive, closed-loop stimulation system. This work concerns the first phase of the study (titration phase), which was focused on the evaluation of the technical feasibility of the proposed closed-loop method as well as the definition of optimal control parameters.

12 patients were included in this first phase, from two centers in France: The University Hospitals of Grenoble and Tours. Patients were eligible for this acute study if they had a history of severe obstructive sleep apnea assessed by polysomnography (PSG) testing within the past 6 months (Apnea-hypopnea index (AHI) > 30 episodes/h and 80% obstructive events). All patients underwent a full standard PSG which was used as a gold standard (Brainbox EEG-1042, Oxymeter Delta PTT II, software Coherence version 6.1.3.405, Braebon Ultima Airflow Pressure

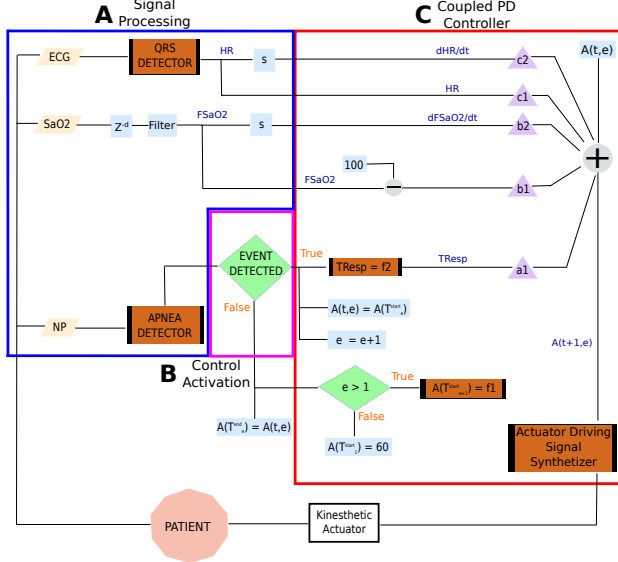


Figure 1. Diagram of the proposed closed-loop control. Signals presented as inputs to the control loop are: nasal pressure (NP), oxygen saturation (SaO2) and electrocardiogram (ECG). ECG and NP signals pass through a QRS and an apnea detector, respectively, in order to determine the heart rate signal (HR) and the TResp signal which corresponds to the time passed into an apnea/hypopnea event. The control coefficients are represented as a_1, b_1, b_2, c_1, c_2 . T_e^{start} and T_e^{end} are the beginning and the end of each detected respiratory event e . Finally, A represents the amplitude value to be delivered by the controller.

Sensor, a surveillance camera and a computer). Simultaneously, NP, ECG and SaO2 signals were acquired and processed by the PASITHEA system. During this first phase, control coefficients were tested with borderline values, in order to estimate their impact on the controller.

A qualitative analysis was performed in order to characterize the patients response to the therapy. The analysis was based on the observation of respiratory event duration, SaO2 level and the cardiorespiratory response, along with a second analysis of the controller's behavior.

3. Results

This section will describe the physiological response of a representative patient to the proposed adaptive kinesthetic stimulation therapy. (Figure 2) shows the acquired data for a patients stimulated with the following control parameters: ($a_1 = 0.03, b_1 = 0, b_2 = 0, c_1 = 0.1, c_2 = -2$). The nasal pressure signal (Figure 2-A) is applied as input to the respiratory event detector. The output of the event detector is shown in Figure 2-B (red line). We observe in this example, the detection of a set of apnea events (marked with an "A"), and a set of hypopnea events ("H"). The

stimulation signal, synthesized at the output of the controller and used to drive the kinesthetic actuator is shown in Figure 2-B, blue line. Note that the stimulation is only delivered when a respiratory event is detected and that the amplitude of the Stim signal changes over time, as a function of the physiological response of the patient. The number of bursts delivered depends on the event duration. In this case, the stimulation was able to stop all the respiratory events within the 6.1 seconds, and in most cases, with a limited number of bursts (one or two bursts). It is also important to highlight that the stimulation amplitude converges to a relatively low, stable value around 50%, showing that the controller tends to minimize the delivered stimulation amplitude, while eliciting the desired physiological response. Another effect of the therapy is shown in figure 2-C, where SaO2 signal remains around 95%, showing no hypoxia events (SaO2 level below 90%) due to the reduced duration of the respiratory episodes. Finally, figure 2-D shows the instantaneous heart rate (HR) signal, as detected from the ECG. It can be observed that there are no significant tachycardia events and the mean HR is low despite the number of respiratory events.

4. Discussion

Previous works have studied the possibility of using kinesthetic stimulation to treat sleep apnea, both in adults and infants. Although results from these studies suggest that this therapy may be useful, some limitations persist in order to be applicable in clinical practice. One of these limitations is related to the stimulation parameters that should be used and, in particular, to the stimulation amplitude. Indeed, if a very large stimulation amplitude is used, respiratory events may be stopped more easily but the patient's sleep can be significantly fragmented, while a too low amplitude will provoke no effect on respiratory events. An optimal stimulation amplitude should be defined between these extreme values.

In most previous works, stimulation parameters are constant for all patients and these parameters are defined heuristically from a test population. It seems obvious from previous results that each patient responds differently to a given set of kinesthetic stimulation parameters, implying the need of patient-specific stimulation parameter values. Moreover, changes in patient sleep stages and position during the night may have consequences on the optimal stimulation amplitude.

In this work, qualitative results showed that the controller is technically capable to adapt the stimulation and to converge to a minimum patient-specific amplitude, which is sufficient to elicit the desired physiological response. These results are encouraging concerning the feasibility of implementing this controller in therapy. However, further studies are necessary to evaluate the effect of the therapy,

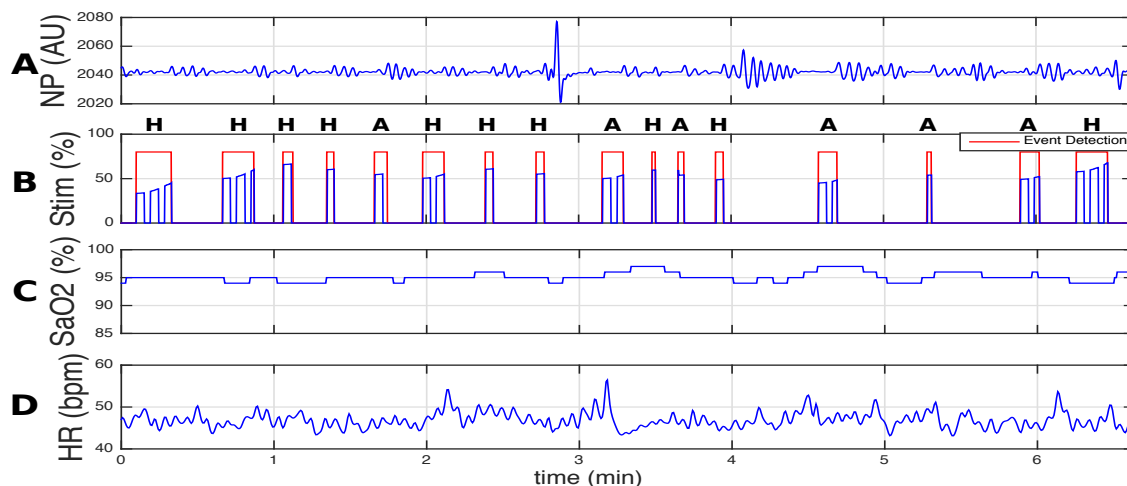


Figure 2. Cardiorespiratory response to adaptive kinesthetic stimulation. A) nasal pressure (NP), B) output of the respiratory event detector along with the amplitude signal of the kinesthetic stimulation (Stim), C) oxygen saturation (SaO₂) and D) instantaneous heart rate (HR), as detected from the ECG.

performing a statistical comparison in the duration and frequency of the SAS events, as well as an analysis of the sleep structure of these patients. These analysis will be performed after the second phase of the EKINOx study. An important aspect that was observed during phase 1 is that the effectiveness of the therapy decreases as the night progresses. We hypothesize that the reason of this loss of effectiveness is due to a reduction of the mechanical coupling between the actuator and the patient's skin throughout the night.

5. Conclusion

This paper presented a novel control system for real-time detection and adaptive therapy delivery through kinesthetic stimulation, directed to patients suffering from SAS. Preliminary results of the effect of the adaptive stimulation shown in this work are very encouraging and they offer valuable information on the feasibility of the implementation of this controller in the therapy. Further works are directed to the clinical evaluation of this device.

6. Acknowledgment

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